

Article

## Electrical and Optical Properties of Fluorine Doped Tin Oxide Thin Films Prepared by Magnetron Sputtering

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**Abstract:** Fluorine doped tin oxide (FTO) coatings have been prepared using the mid-frequency pulsed DC closed field unbalanced magnetron sputtering technique in an Ar/O<sub>2</sub> atmosphere using blends of tin oxide and tin fluoride powder formed into targets. FTO coatings were deposited with a thickness of 400 nm on glass substrates. No post-deposition annealing treatments were carried out. The effects of the chemical composition on the structural (phase, grain size), optical (transmission, optical band-gap) and electrical (resistivity, charge carrier, mobility) properties of the thin films were investigated. Depositing FTO by magnetron sputtering is an environmentally friendly technique and the use of loosely packed blended powder targets gives an efficient means of screening candidate compositions, which also provides a low cost operation. The best film characteristics were achieved using a mass ratio of 12% SnF<sub>2</sub> to 88% SnO<sub>2</sub> in the target. The thin film produced was polycrystalline with a tetragonal crystal structure. The optimized conditions resulted in a thin film with average visible transmittance of 83% and optical band-gap of 3.80 eV, resistivity of  $6.71 \times 10^{-3} \Omega \cdot \text{cm}$ , a carrier concentration ( $N_d$ ) of  $1.46 \times 10^{20} \text{ cm}^{-3}$  and a mobility of  $15 \text{ cm}^2/\text{Vs}$ .

**Keywords:** fluorine doped tin oxide; oxide powder target; pulsed DC magnetron sputtering; thin films; transparent conductive oxide; photovoltaic cells

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## 1. Introduction

Un-doped tin oxide ( $\text{SnO}_2$ ), is a wide band-gap semiconductor ( $E_g > 3$  eV) that exhibits high optical transparency ( $T \geq 85\%$ ) and an n-type character due to oxygen vacancies [1]. The electrical conductivity of the material can be largely enhanced by doping with foreign impurities. The most favoured dopants are antimony which substitutes the tin cations or by fluorine via substituting the oxygen atoms [1].

Fluorine doped tin oxide (FTO) exhibits good visible transparency owing to its wide band-gap, while retaining a low electrical resistivity due to the high carrier concentration ( $N_d$ ) caused by the oxygen vacancies and the substitutional fluorine dopant [2]. FTO is mechanically, chemically and electrochemically stable [3], and it is utilized in numerous technologies including; thin film solar cells [4], dielectric layers in low emissivity coatings for windows [5], in gas sensors applications [6] and in liquid crystal displays [7]. There are a number of methods/techniques to grow  $\text{SnO}_2$  (either doped or un-doped) films, including chemical vapor deposition [8], pulsed laser deposition [9], DC reactive sputtering [10] and spray pyrolysis [11].

Some techniques require a high substrate temperature to deposit the film, which can often cause the formation of intermediate semiconductor oxide layers at the film boundary [12]. Any post-treatment of the films, such as annealing, also poses additional operational costs and reduced throughput. A few attempts have been made to sputter FTO from solid targets using techniques such as RF magnetron sputtering [13]. More recent work deals with DC reactive magnetron sputtering using a metallic tin target and various plasma atmospheres such as  $\text{Ar}/\text{O}_2/\text{CF}_4$  [10],  $\text{Ar}/\text{O}_2/\text{Freon}$  [14].

This paper presents a unique alternative way to deposit FTO by mid-frequency (100–350 kHz) pulsed DC magnetron sputtering from loosely packed (as opposed to sintered or pressed) blended powder targets. Thin films have been produced at a low deposition temperature ( $\sim 170$  °C process heating and no post deposition treatment) and a relatively high deposition rate of  $27 \text{ nm} \cdot \text{min}^{-1}$ . Such a technique has been used for the production of other TCO thin films [15], such as ZnO [16] and Al doped ZnO [17].

This technique has further advantages over conventional DC or RF sputtering from solid metallic or ceramic targets, such as employing a closed field unbalanced magnetron configuration and pulsed sputtering to enhance the sputtering rate, benefit from low deposition temperatures, suppress arcs and produce dense homogenous films [18]. Čada *et al.* measured the power density at the substrate in order to assess the interaction between the plasma and the substrate and quantify the energy balance. They concluded that pulsing the magnetron discharge provides higher energy transfer to the growing film this, in turn, produces denser film structures [19].

The use of pulsed DC mode configuration during the sputtering of the oxide powder targets means there is no need for reactive process control equipment and no need for a RF matching network. The powder is loosely packed (as opposed to sintered or pressed), so target cracking is avoided and, most importantly, the target composition can be readily varied. The powder target approach is a cheap and efficient means of investigating and optimizing the properties of multi-component materials, compared to using metallic or ceramic targets [20].

In this work, fluorine doped tin oxide coatings were produced from blended  $\text{SnO}_2$  and  $\text{SnF}_2$  powder targets and the effect of different fluorine doping levels was investigated. The chemical composition, structural, electrical and optical properties of the FTO coatings sputtered in an argon/oxygen gas mixture at different deposition conditions is reported.

## 2. Experimental Section

FTO thin films were deposited onto standard size (5 mm by 25 mm, 1 mm thick) microscope glass slides using a mid-frequency pulsed DC magnetron sputtering technique from loose powder targets. Different fluorine doping levels were prepared in the tin oxide powder targets in order to study the effect of doping level on the structure and opto-electrical properties of the thin films. The mass ratios of the different target compositions are presented in Table 1.

**Table 1.** Target compositions by mass for the production of tin oxide and fluorine doped tin oxide thin films.

Powder target ID	Compound powder target mass (g)	
	Tin oxide	Tin fluoride
SnO <sub>2</sub>	60.0	0
SnO <sub>2</sub> :F1	57.5	2.5
SnO <sub>2</sub> :F2	52.7	7.3
SnO <sub>2</sub> :F3	46.1	13.9
SnO <sub>2</sub> :F4	43.2	16.8

Each target was produced by mixing appropriate quantities of SnO<sub>2</sub> (particle size: 325 mesh, purity 99.99%; source: Alfa Aesar, Heysham, UK) with SnF<sub>2</sub> (particle size: 250 mesh, purity 97.5%; source: Alfa Aesar, Heysham, UK) to make a total mass of 60 g. The powder target material was inserted into a glass bottle, which was placed on a tumble rotator for several hours to ensure the blending of the powders. The blended powder target material was then distributed across a 2 mm recessed circular copper backing plate on the magnetron plate and was tamped down using a 1 kg steel cylinder to ensure uniformity of the target surface and also to ensure the power is dense for a better thermal and electrical conductivity. No additional adjustments were carried on the target surface such as sintering the powders or pressing with excessive force.

The magnetron, which is strongly unbalanced, has a diameter of 180 mm to provide a reasonable area of uniform deposition on the substrate. A full description of the deposition system has been given previously [16,17,21,22].

The thin films were pre-cleaned with an ultrasonic cleaning process using methanol solution. The substrates were then air-dried and mounted on the substrate holder and positioned vertically above the target at a separation of 110 mm in the chamber.

The chamber was evacuated to a base pressure of  $2.1 \times 10^{-4}$  Pa before initially introducing argon gas at a working pressure of 0.24 Pa to perform a substrate and target surface cleaning process. The substrate holder was connected to a RF power supply (RFX-600, Advanced Energy, Little Hampton, UK) which was set to  $0.13 \text{ W}\cdot\text{cm}^{-2}$  for a period of 10 min to further clean any contamination from the substrate via plasma etching prior to deposition. Simultaneously, the target surface was cleaned using an Advanced Energy DC Pinnacle Plus power supply with operating conditions; pulsing frequency of 200 kHz, duty cycle of 90% and sputtering power density of  $0.2 \text{ W}\cdot\text{cm}^{-2}$  for a period of 10 min. After the cleaning process, the oxygen gas was added to yield an Ar/O<sub>2</sub> ratio of 9:1 at a total working pressure of 0.54 Pa. During this time, the substrate was shuttered in order to prevent deposition.

During the deposition, the shutter was opened and the magnetron discharge was pulsed at 200 kHz to provide a power density of  $1.6 \text{ W} \cdot \text{cm}^{-2}$ , at 90% duty cycle (pulse off time = 0.5  $\mu\text{s}$ ). These conditions were chosen to produce stable arc free deposition conditions.

The deposition period of all the experiments was set to 15 min. The optimum deposition rate of  $27 \text{ nm} \cdot \text{min}^{-1}$  was achieved through a trial of different pulsing frequency, duty cycle and target to substrate distance, using the  $\text{SnO}_2$  powder target. The achieved deposition rate is higher than that reported in other deposition techniques such as spray pyrolysis [11]. The deposition rate for the different powder targets was found not vary during this study. The synthesis temperature during the deposition of the thin film was measured to be below  $170 \text{ }^\circ\text{C}$  at the substrate using a platinum thermal resistor sensor.

The thickness of the thin films was determined using a stylus profilometer (Dektak IID, Veeco, Cambridgeshire, UK). A piece of Kapton tape was placed on the microscope glass slide, which was removed after the deposition to give a step height. This step height was measured at four different points on each sample and a thickness variation of  $\pm 5\%$  was observed. The structural properties were determined using X-ray diffraction with a PANalytical XPert<sup>3</sup> diffractometer (PANalytical, Cambridge, UK) using  $\text{Cu K}\alpha_1$  radiation according to the Bragg-Brentano configuration. The  $\theta$ - $2\theta$  mode XRD measurements were collected between  $20^\circ$  and  $70^\circ$ . The thin film compositions and morphology were determined using energy-dispersive X-ray spectroscopy (EDS) with the electron-beam energy set to 7 keV to determine the fluorine concentration (EDAX Trident, Ametek, Leicester, UK) and FE-SEM. The electrical properties including mobility, resistivity and carrier concentration ( $N_d$ ) of the films were measured using a Hall Effect measurement system (Ecopia HMS-3000, Ecopia, South Korea). The optical properties were determined using a spectrophotometer (Ocean Optics USB2000+, Ocean Optics, Wokingham, UK) with a wavelength range of 300–900 nm. An uncoated glass slide was used as a reference for transmittance measurements. The transmittance data was used to calculate the absorption coefficient ( $\alpha$ ); a plot of the variation of the absorption coefficient against the photon energy ( $h\nu$ ) was used to determine the optical band-gap from extrapolation of the linear portion of the curve to zero absorption [23].

### 3. Results and Discussion

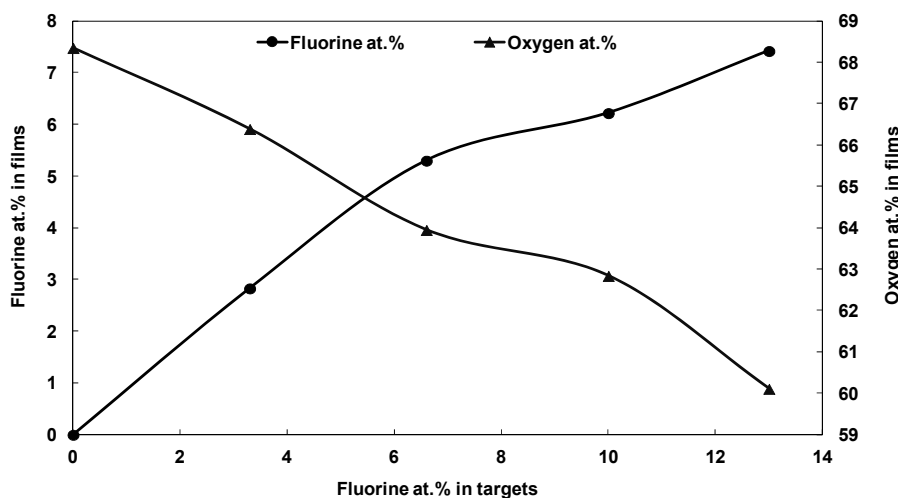
#### 3.1. Elemental Analysis

The EDS absolute data from the analysis of the FTO films is given in Table 2. It is important to note that any oxygen detected from the glass substrate was not taken into consideration during the analysis of this study, because the energy of the EDS beam was optimized to be low enough not to detect the elements of glass such as Si and Ca and it was, therefore, also assumed not necessary to consider the oxygen arising from the glass substrate. The analysis of the un-doped tin oxide film shows a composition of 31.7 at.% tin and 68.4 at.% oxygen which is close to stoichiometric  $\text{SnO}_2$ . It was observed that the fluorine content in the doped thin films is in the range of 0–7.4 at.%, which is low in comparison to the amount of fluorine incorporated into the powder targets (0–13 at.%). This can be explained by the fact that fluorine is a light element ( $Z = 9$ ) and may be more readily scattered during gas phase transport through the high density plasma [19].

**Table 2.** Compositional analysis of the powder targets and subsequent tin oxide and fluorine doped tin oxide.

Sample ID	Element at.% in targets			Element at.% in films			Film thickness (nm)
	O	F	Sn	O	F	Sn	
SnO <sub>2</sub>	66.7	0.0	33.4	68.4	0.0	31.7	403
SnO <sub>2</sub> :F1	63.3	3.3	33.3	66.4	2.8	30.8	410
SnO <sub>2</sub> :F2	60.0	6.6	33.3	64.0	5.3	30.7	405
SnO <sub>2</sub> :F3	56.7	10.0	33.2	62.8	6.2	30.9	415
SnO <sub>2</sub> :F4	53.4	13.0	33.3	60.1	7.4	32.5	395

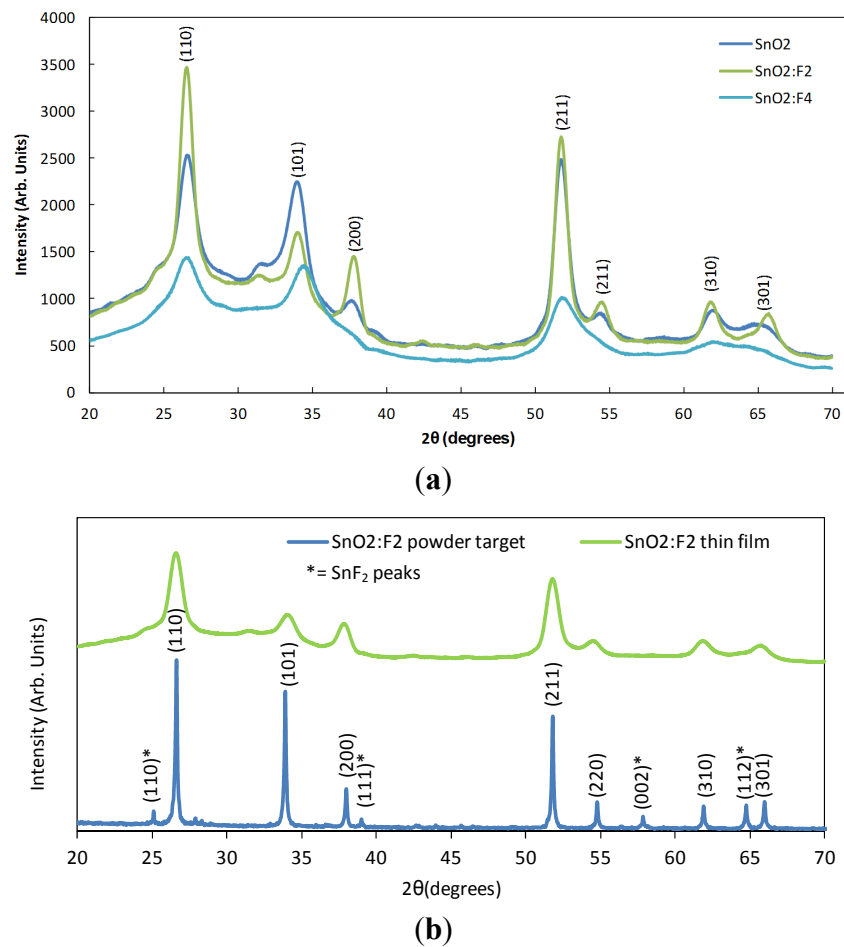
Figure 1 depicts the relationship between the fluorine and oxygen atomic content incorporated in the film, both as a function of the fluorine content of the target. It was observed that the fluorine to oxygen ratio increased with the increase in the fluorine content in the thin film. This indicates that the fluorine was successfully incorporated into the tin oxide, as each F<sup>-</sup> anion substitutes an O<sup>2-</sup> anion in the lattice. This is attributed to the fact that fluorine is the most favored oxygen substitute, because the ionic size of fluorine (F<sup>-</sup>:0.133 nm) is closely matched to that of oxygen (O<sup>2-</sup>:0.132 nm) [24].

**Figure 1.** Energy-dispersive X-ray spectroscopy (EDS) analysis of fluorine and oxygen atomic content in the fluorine doped tin oxide (FTO) films as a function of fluorine atomic content in the target.

### 3.2. Structural Properties

The crystal structures of the SnO<sub>2</sub> and SnO<sub>2</sub>:F thin films were analysed using X-ray diffraction over the range 20° to 70° 2θ. The XRD patterns for the SnO<sub>2</sub>, SnO<sub>2</sub>:F2 and SnO<sub>2</sub>:F4 (chosen as a representative example of the doped films) films are presented in Figure 2a. Also, Figure 2b shows a comparison between the spectra of the bulk powder target SnO<sub>2</sub>:F2 and the spectra of the as deposited SnO<sub>2</sub>:F2 thin film. The diffraction angle (2θ), Miller indices, grain size and texture coefficient for all the thin films are presented in Table 3.

**Figure 2.** X-ray diffraction patterns showing the (a) effect of doping on the crystallography of SnO<sub>2</sub>, SnO<sub>2</sub>:F2 and SnO<sub>2</sub>:F4 thin film samples on glass substrates, and (b) the comparison between the spectra of the SnO<sub>2</sub>:F2 bulk powder target and the SnO<sub>2</sub>:F2 thin film sample.



**Table 3.** Diffraction angle ( $2\theta$ ), the miller indices ( $hkl$ ), grain size ( $D$ ) and the texture coefficient ( $P$ ) of FTO thin films.

Sample ID	$2\theta$ (°)	Peak ( $hkl$ )	Lattice parameters		Grain size $D$ (nm)	Texture coefficient $P$
			$a$ (Å)	$c$ (Å)		
SnO <sub>2</sub>	26.6	110	4.74	3.35	15	0.48
	37.7	200	4.75	2.37	24	0.42
	51.7	211	4.32	1.77	22	1.27
SnO <sub>2</sub> :F1	26.5	110	4.79	3.39	28	0.73
	37.8	200	4.77	2.38	23	0.95
	51.6	211	4.34	1.77	34	1.48
SnO <sub>2</sub> :F2	26.5	110	4.79	3.38	31	0.77
	37.8	200	4.81	2.4	38	1.11
	51.7	211	4.32	1.77	33	1.31
SnO <sub>2</sub> :F3	26.6	110	4.77	3.38	13	0.47
	37.7	200	4.78	2.39	14	0.6
	51.6	211	4.34	1.77	15	1.01
SnO <sub>2</sub> :F4	26.6	110	4.81	3.4	9	0.3
	51.4	211	4.35	1.78	7	0.49

From Figure 2a, it can be observed that the films exhibited XRD patterns with diffraction peaks corresponding to the (110), (101), (200), (211), (301), and (310) peaks of the rutile SnO<sub>2</sub> pattern [25]. The presence of these peaks indicates that all the films were found to be of the cassiterite type with a polycrystalline structure. No other diffraction lines that correspond to other tin oxide or tin fluoride structures were detected in the thin film spectra, which indicates the O atoms were replaced by F atoms in the SnO<sub>2</sub>:F thin films [26]. It was evident from the comparison between the powder target spectra and that of the thin film sample, that the peaks marked corresponding to the SnF<sub>2</sub> spectra marked with an asterisk were not present in the deposited thin film, which suggests that the fluorine atoms are fully incorporated into the tin oxide lattice. In addition, there was no significant shift in the peak positions of all the developed thin films, which probably implies that fluorine doping, did not introduce any significant stress in the films. It is apparent from Figure 2a that the un-doped SnO<sub>2</sub> sample has a lower intensity in comparison to the sharper more intense peaks of SnO<sub>2</sub>:F<sub>2</sub> sample. In another words, the crystallinity of the SnO<sub>2</sub> samples were improved with the fluorine incorporation (2.8 to 5.3 at.%). In the present investigation, the intensity of the (200) plane ameliorates with the increase in the fluorine concentration up to 5.3 at.% and then deteriorated with fluorine concentration up to 7.4 at.% (sample SnO<sub>2</sub>:F<sub>4</sub>), a similar behaviour was observed by Moholkar *et al.* [27]. It is therefore concluded that the fluorine content strongly effects the structure of the SnO<sub>2</sub>, as observed elsewhere [28].

Thin films deposited via magnetron sputtering, usually exhibit a preferred orientation because the sputtered atoms arrive at the substrate via limited pathways, therefore promoting the formation of a columnar microstructure. A preferred orientation can also be affected by experimental parameters, such as the growth temperature [29,30], coating thickness [31] and fluorine doping level [9,11].

The intensity of the *hkl* reflection pattern can be utilised to determine the orientation of the grains or the volume of crystallites within that particular *hkl* plane parallel to the surface sample.

The degree of the preferred orientation of the thin films can be estimated by comparing the relative intensities of the measured peaks. A texture coefficient TC (*hkl*) is calculated using the Harris analysis technique shown in Equation (1) [32],

$$TC(hkl) = \frac{I(hkl)}{I_o(hkl)} \times \left[ \frac{1}{n} \sum_{i=1}^n \frac{I(hkl)}{I_o(hkl)} \right]^{-1} \quad (1)$$

where *I* is the measured intensity of the peak, *I<sub>o</sub>* is the theoretical intensity obtained from the JCPDS powder diffraction file and *n* is the number of peaks. The texture coefficients for the (110), (200) and (211) peaks are shown in Table 3.

It is apparent from Table 3 that the coatings tend to have a (211) preferred orientation or texture (TC > 1). FTO coatings grown by other techniques suggest that the (200) peak was most influenced by fluorine doping [18]. Although the TC of the (200) peak varies with fluorine content, becoming a maximum of 1.11 at 5.3 at.% F, it still remains below the TC for the (211) peak.

The grain sizes of the crystallites were calculated using the Scherrer equation shown in Equation (2) for the (110), (211) and (200) peaks [33]. It is important to note that a lattice strain de-convolution was not considered during the calculation.

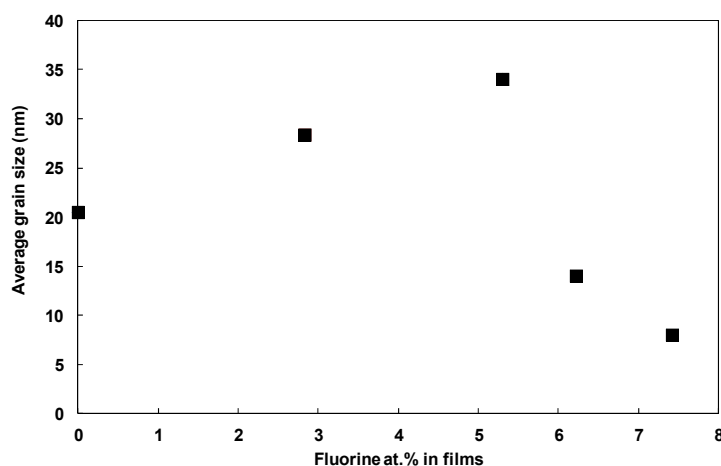
$$D = \frac{0.9\lambda}{\beta \cos \theta} \quad (2)$$

where  $D$  is the grain size,  $\lambda$  is the wavelength of the X-ray source used,  $\beta$  is the full width half maximum (FWHM) of the specific peak,  $\theta$  is the Bragg angle of that peak. The calculated values are presented in Table 3.

The average of the grain sizes for the (110), (200) and (211) peaks is shown in Figure 3. It was observed that the mean crystallite size followed a progressive incremental trend with increasing fluorine content up to 5.3 at.% (from 20 nm to 34 nm). Similar trends were observed by Mientus *et al.* which showed an increase in the grain size from 12 to 25 nm [10], also similar trend was observed by Kim *et al.* which showed an increase in the grain size from 4 to 30 nm [9]. Beyond 5.3 at.% of fluorine in the thin film, there was a reduction in the crystallite size, which may be due to the excess fluorine within the tin oxide lattice. The implication being that 5.3 at.% of fluorine in the lattice was the optimum composition, of those tested, for grain growth.

The calculated values for the lattice parameters “ $a$ ” and “ $c$ ” for SnO<sub>2</sub> thin films are 4.74 Å and 3.35 Å for the (110) peak which are in reasonable agreement with the standard data ( $a = 4.73$  Å,  $c = 3.18$  Å) [25].

**Figure 3.** Average grain size variation as a function of fluorine atomic content in the FTO thin films.



### 3.3. Electrical Properties

To characterise the electrical properties of the thin films, Hall Effect probe measurements in a Van der Pauw configuration at room temperature were employed [34]. Figure 4 presents the electrical behaviour of the thin films as a function of the fluorine content. The values for the carrier concentration ( $N_d$ ) were reported to be negative, however, the absolute value was plotted to present the trend of the data.

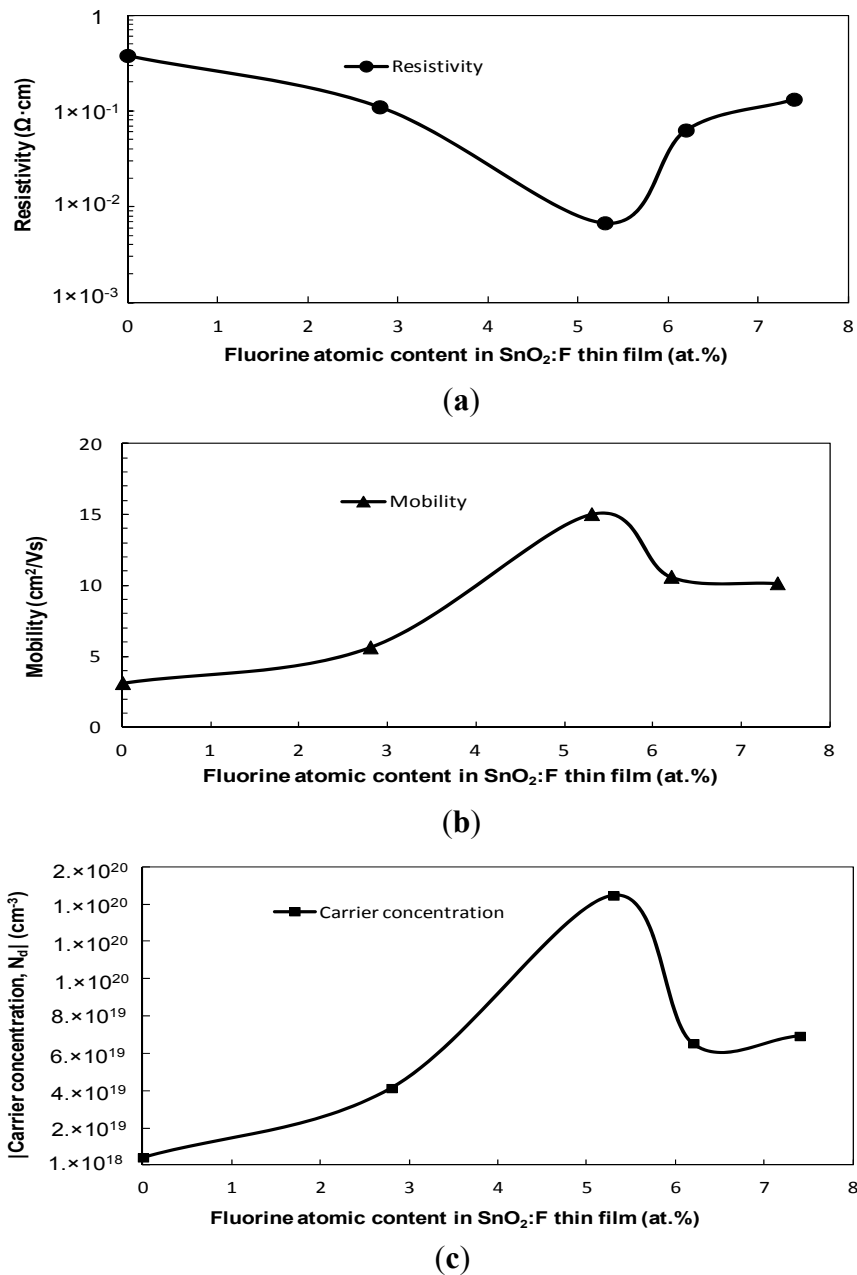
Resistivity and mobility values of  $3.71 \times 10^{-1} \Omega \cdot \text{cm}$  and  $3.1 \text{ cm}^2/\text{Vs}$  and a corresponding carrier concentration ( $N_d$ ) of  $5.5 \times 10^{18} \text{ cm}^{-3}$  were obtained for un-doped SnO<sub>2</sub>. These values are similar to those reported elsewhere [10,12]. It was observed from the carrier concentration ( $N_d$ ) data that the FTO thin films exhibit n-type conductivity which is also achieved by other deposition techniques including spray pyrolysis and PLD [2,9].

It was observed from Figure 4, that the best electrical properties were achieved with a fluorine concentration of 5.3 at.%, corresponding to a resistivity of  $6.71 \times 10^{-3} \Omega \cdot \text{cm}$ , mobility of  $15.1 \text{ cm}^2/\text{Vs}$  and a carrier concentration ( $N_d$ ) of  $1.46 \times 10^{20} \text{ cm}^{-3}$  for the films. Similar results were achieved by PLD at a



deposition temperature of 300 °C [9]. The improvement in the electrical properties is attributed to the larger grain size observed at this composition [9]. In addition, the hybrid orbital configuration of fluorine and oxygen are  $2S^22P^5$  and  $2S^22P^4$ , respectively, indicating that fluorine atoms promote one free electron/molecule when it sits in place of oxygen. As the ionic radius of F (1.36 Å) is slightly lower than that of  $O^{2-}$  (1.40 Å), so the fluorine atoms are more electronegative than the oxygen atoms, therefore the fluorine substitutes the oxygen sites more easily [35]. This phenomenon leads to higher carrier concentration, which is shown in Figure 4. Similar trends were observed in [4].

**Figure 4.** Variation of: (a) resistivity in logarithmic scale; (b) mobility; and (c) absolute carrier concentration of FTO thin films as a function of fluorine atomic content.



Increasing the fluorine content in the film beyond 5.3 at.% resulted in a degradation of the electrical properties. This is probably attributed to the solubility limit of fluorine into the tin oxide lattice [11], and probably the cause for the reduction in the grain size, as observed in Table 3 [3]. The excess fluorine atoms do not occupy the correct position within the lattice, which leads to disorder of the structure, grain boundary scattering and therefore to a decrease in the free carrier concentration ( $N_d$ ) and mobility and an increase in the resistivity ( $7.04 \times 10^{19} \text{ cm}^{-3}$ ,  $10.15 \text{ cm}^2/\text{Vs}$  and  $1.31 \times 10^{-1} \Omega \cdot \text{cm}$ , respectively). The effect of the fluorine content on the electrical properties of FTO was investigated by Elangovan *et al.*, who reported the degradation in the electrical properties is probably due to the solubility limit of fluorine content in the thin film [11]. Kim *et al.* found that a saturation carrier concentration ( $N_d$ ) is achieved due to the formation of Sn-F complexes in the grain boundaries when using higher than 10 wt.% of  $\text{SnF}_2$  in target [9]. The electrical results depicted in this study indicate that the mobility and the carrier concentration ( $N_d$ ) were limited by the solubility limit of fluorine content in the film. This behaviour is also observed by Elangovan *et al.* [11].

### 3.4. Optical Properties

The optical transmittance and the direct band-gap properties of  $\text{SnO}_2:\text{F}$  films as a function of fluorine content in the thin films are presented in Figures 5 and 6, respectively. The transmittance data of each sample was recorded three times and an average taken. The optical transmittance ( $T$ ) was averaged over the wavelength range of 300–900 nm, and the absorption coefficient ( $\alpha$ ) was determined by using Equation (3),

$$T \approx e^{-\alpha t} \quad (3)$$

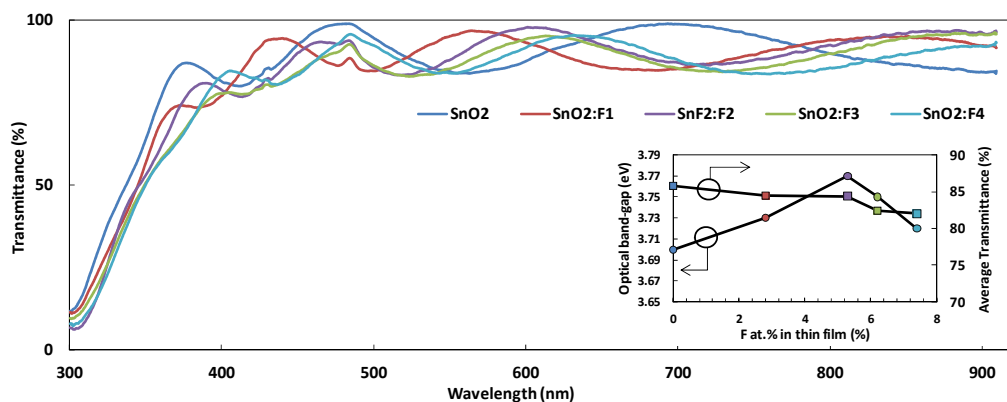
where,  $t$  is the thickness of the film. The absorption refers to the excitation of an electron from the valence band to the conduction band. The absorption coefficient was then used to estimate the direct optical energy band-gap ( $E_g$ ) using the relation shown in Equation (4),

$$\alpha h\nu = C (h\nu - E_g)^{1/2} \quad (4)$$

where  $h$  is Planck's constant,  $\nu$  is the frequency of the incident photon,  $C$  is a constant for direct transition and  $\alpha$  is the absorption coefficient. The direct optical energy band-gap ( $E_g$ ) was estimated by extrapolating the linear portion of the curve  $(\alpha h\nu)^2$  against  $(h\nu)$  for direct allowed transition to the point where  $\alpha h\nu = 0$  [36].

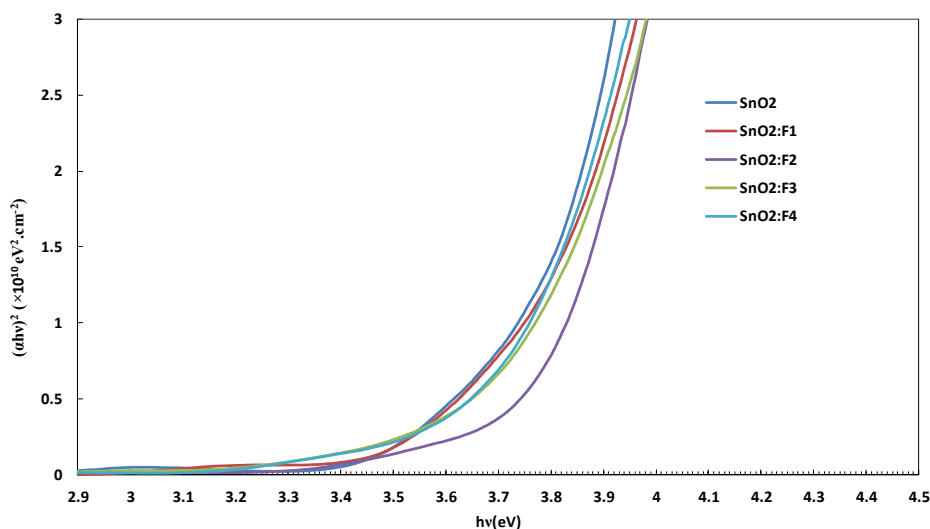
The optical transmission spectra recorded in the wavelength range of 300 to 900 nm are presented in Figure 5. High transparency in the visible range ( $82 < T_{\text{vis}} < 85$ ) was observed, in accordance with the requirements for TCO applications (80%) [37]. This can be associated with good structural homogeneity. It is evident from the Figure 5; the average visible transmittance is not influenced much for different doping levels of fluorine, similar behaviour was also observed in [35] and [38]. However, a slight decrease in the transmission is probably due to the decrease in the oxygen vacancies as perceived in the EDS data shown in Table 2. The insert in Figure 5 is for the convenience of the reader to give a quick average view of the transmission and the direct optical band-gap against the change in the fluorine concentration in the thin film. The sharp decrease in the transmission in the UV range of the spectrum is related to the light absorption edge [39]. It is also possible to notice that both the un-doped and the doped films showed interference fringes pattern, suggesting that there is little scattering losses at the surface.

**Figure 5.** The optical transmittance of FTO thin films as a function of fluorine atomic content. The insert shows the variation in optical band-gap and the average transmittance across the  $300 \leq \lambda \leq 900$  nm with change in fluorine concentration in thin film.



The direct band-gap for un-doped tin oxide was estimated to be 3.70 eV, which increased slightly to a value of 3.77 eV at a fluorine content of 5.4 at.% in the film as observed in Figure 6. The direct band-gap values obtained in this work are slightly higher than the direct band-gap values of 3.17–3.45 eV reported in [11] and slightly lower than the band-gap values of 4.0–4.25 eV reported in [9]. This variation is probably attributed to the different concentration of fluorine used in the film, the thickness variation and the experimental variables such as working pressure and deposition temperature.

**Figure 6.** The direct allowed transition of FTO thin films as a function of fluorine atomic content.



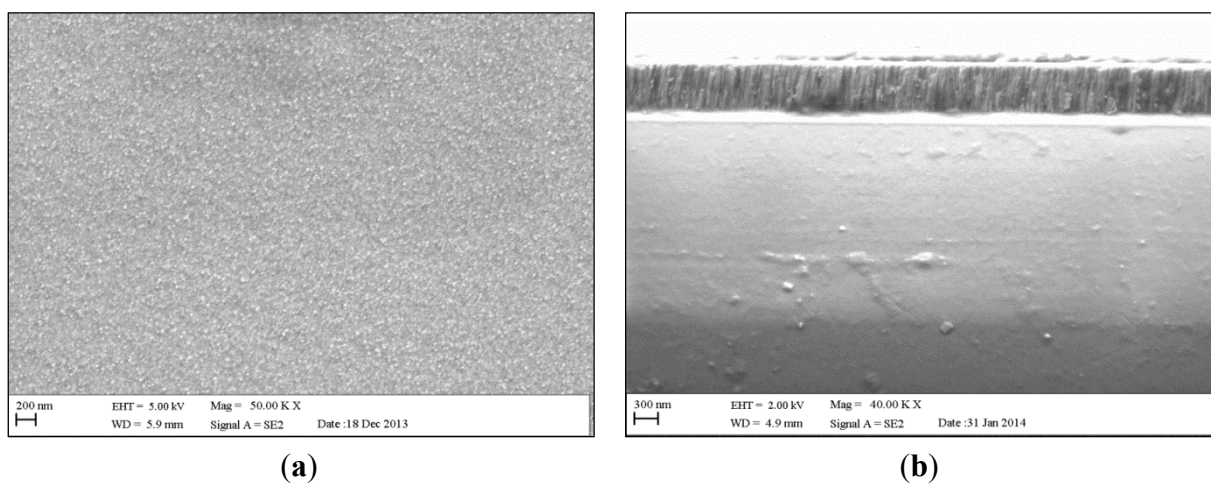
Generally, the band-gap energy for doped metal oxides films is higher than that of the un-doped type. This is because the energy gap between the valence band and the lowest empty state in the conduction band is found to increase due to the filling of low lying energy levels in the conduction that is caused by the increase in the carrier concentration (Burstein-Moss effect) [37]. The shift in the band-gap can also be related to the variation in the mean crystallite size, the internal stress or due to the free carrier concentration [40].

### 3.5. Morphological Properties

Figure 7a,b shows the surface area and the cross-section SEM morphologies of SnO<sub>2</sub>:F<sub>2</sub> film, respectively. The film has a compact and dense homogenous surface characterised by small grains. The small grains observed in Figure 7a are probably a result of the low deposition temperature. Consonni *et al.* studied the effect of deposition temperature and observed an increase in the mean grain size from 60 to 127 nm as the growth temperature raised from 360 to 460 °C.

The thickness of the film was measured to be about 410 nm, which is in a good agreement with the Dektak profilometer measurements. The cross-sectional images show that the thin film has a dense columnar grained structure normal to the surface of the substrate.

**Figure 7.** (a) Surface and (b) cross-sectional SEM morphologies of SnO<sub>2</sub>:F<sub>2</sub> thin film.



## 4. Conclusions

Transparent conductive oxide SnO<sub>2</sub>:F thin films have been deposited on glass substrates by the pulsed DC magnetron sputtering technique in an Ar/O<sub>2</sub> atmosphere using loosely packed blended powder targets. The thin films were grown at a deposition rate of 27 nm·min<sup>-1</sup> and a deposition temperature below 170 °C. It was determined that 5.3 at.% of fluorine incorporated into the film gave the best electrical behavior. In addition, the XRD structural analysis showed that the crystallinity of the SnO<sub>2</sub> samples were improved with the fluorine incorporation and the intensity of the (200) plane ameliorated with the increase in the fluorine concentration up to 5.3 at.% found in the thin film. The average optical transmittance achieved for this coating was 83% across a range of 300 ≤ λ ≤ 900 nm. The detailed analysis of the electrical properties of the thin film as a function of the fluorine doping level revealed that a resistivity as low as 6.71 × 10<sup>-3</sup> Ω·cm was obtained with a fluorine content of 5.3 at.%.

This work has shown the ability to grow transparent conductive oxide SnO<sub>2</sub>:F thin films using a cost effective (no post annealing of samples, and high deposition rate) and environmentally friendly method (no fluorine gas is used and no toxic affluent is produced). This technique is of great advantage for studying the properties of multicomponent materials and identifying optimum compositions.

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## Author Contributions

Ziad Y. Banyamin conducted the experiments and was the lead author. Peter J. Kelly and Glen West were the supervisory team for the experimental programmes described here. Jeffery Boardman acted as the external consultant.

## Conflicts of Interest

The authors declare no conflict of interest.

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